

SYNERGISTIC EFFECT BETWEEN CO₂ AND H₂O ON BIOMASS CHEMICAL LOOPING GASIFICATION WITH HEMATITE AS OXYGEN CARRIER

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ABSTRACT

A computational fluid dynamic (CFD) model has been developed for the fuel reactor of a chemical looping gasification (CLG) system with biomass as fuel and natural hematite as oxygen carrier (OC). By coupling the fluid dynamics and the chemical kinetics, the multiphase continuum model is able to describe the motion of gas and solid phases and the heterogeneous reactions between them, which take place in a bubbling fluidized bed reactor. The simulated average concentrations of five gas species fit the experimental data provided in the literature quite well, with a deviation for each gas component lower than 2%. This verified model is then applied to investigate the effects of various gasifying agents on the compositions of syngas. The results show that the biomass CLG performance is significantly improved in the presence of CO₂/H₂O and their mixture. Furthermore, synergistic effect of CO₂/H₂O mixture can be observed based on the evolution of char mass within the reactor.

Keywords: biomass gasification, chemical looping, synergistic effect, gasification atmosphere

1. INTRODUCTION

As a renewable and carbon neutral energy source, biomass is regarded as one of the promising solutions to cope with fossil fuel depletion and global warming by mitigating the CO₂ emissions in the atmosphere [1]. Increasing attention has been paid to various energy conversion technologies for biomass, among which gasification is undoubtedly a favorable one that can convert the solid fuel into valuable synthesis gases, including H₂ and CO [2]. Moreover, researchers have

found that gasification process will show better performance in the presence of H₂O/CO₂ or their mixture, which are excellent gasifying agents for producing high quality syngas [3].

The chemical looping method is considered as one of the clean energy conversion technologies and has been extensively studied in the fields of combustion and gasification with various kinds of fuels [4,5]. Unlike the traditional gasification technologies, a chemical looping gasification (CLG) system consisting of two reactors (air reactor and fuel reactor) adopts the circulating solids called oxygen carrier (OC) instead of air or pure O₂ to be the oxygen source and convert solid fuels into syngas. The application of two reactors avoids the direct contact between fuel and air, thus eliminating both the dilution of syngas by N₂ and the potential generation of NO_x. Previous research has experimentally proved that the presence of metal oxides can evidently promote the biomass conversion and obtain higher efficiency in comparison to the conventional gasification process [6].

Numerical simulation is a useful approach to analyze the interaction between hydrodynamics and chemical kinetics. Li et al. [7] conducted a numerical investigation of syngas production in a fixed bed reactor, where the effects of operating temperature and steam ratio were also evaluated in terms of gas yield and gasification efficiency. Despite the considerable impact of CO₂ on char conversion [3], there have been few reports on the modelling of CLG process with CO₂ as gasifying agent.

The objective of this study is to develop a CFD model to simulate a CLG fuel reactor with biomass as fuel. The model is validated by the experimental results, after which it is applied to examine the effects of H₂O, CO₂ and

their mixture on the solids conversion as well as the gasification performance.

2. METHODOLOGY

2.1 CFD model

The multi-fluid model has been employed in the present work. The governing equations for mass, momentum, energy and species transport of the Eulerian approach are the same as those used in the published reference [8].

2.2 Chemical reaction kinetic model

Table 1

Reaction mechanisms used in this model.

Description	Reaction equation	
Primary pyrolysis	Biomass \rightarrow Char + Wood gas (CH ₄ , C ₂ H ₄ , CO, CO ₂ , H ₂ , H ₂ O) + Tar	(R1)
Secondary pyrolysis	Tar \rightarrow Wood gas (CH ₄ , C ₂ H ₄ , CO, CO ₂ , H ₂ , H ₂ O) + Tar _{inert}	(R2)
Char gasification	C + CO ₂ \rightarrow 2CO	(R3)
	C + H ₂ O \rightarrow CO + H ₂	(R4)
Water-gas shift (WGS)	CO + H ₂ O \rightarrow CO ₂ + H ₂	(R5)
Metal oxide reduction	CH ₄ + 9.75Fe ₂ O ₃ \rightarrow 0.25CO + 0.5H ₂ + 0.75CO ₂ + 1.5H ₂ O + 6.5Fe ₃ O ₄	(R6)
	C ₂ H ₄ + 12Fe ₂ O ₃ \rightarrow CO + CO ₂ + H ₂ + H ₂ O + 8Fe ₃ O ₄	(R7)
	CO + 3Fe ₂ O ₃ \rightarrow CO ₂ + 2Fe ₃ O ₄	(R8)
	H ₂ + 3Fe ₂ O ₃ \rightarrow H ₂ O + 2Fe ₃ O ₄	(R9)

2.3 Initial and boundary conditions

Four cases with different gasification atmosphere are examined in this study, as shown in Table 2. Case 1 is to simulate the experiment of Huang et al. [6] and acts as the base case, in which the volumetric flow of Ar is 1500L/h. For case 2 and 3, the fluidizing gas is a mixture of steam/Ar and CO₂/Ar, respectively, with the same total volume flow rate. Both steam and CO₂ are introduced into the reactor to investigate the synergistic effect during chemical looping gasification in case 4. The natural hematite containing 90 wt.% of Fe₂O₃ is packed inside the reactor with the initial height of 26 mm. The sawdust is continuously fed into the reactor through a drop tube, whose bottom is 30 mm from the porous plate. The operating temperature is set at 840 °C. More details of the experimental setup can be found in [6].

Table 2

Various atmosphere adopted in this study.

Case No.	Gasification atmosphere
1	100% Ar
2	50% H ₂ O + 50% Ar
3	50% CO ₂ + 50% Ar
4	25% H ₂ O + 25% CO ₂ + 50% Ar

The reaction mechanisms adopted for this study are shown in Table 1. The two-step pyrolysis model considering the biomass devolatilization and tar cracking [9] is utilized in this work, with a composition of various gas species determined by the ultimate and proximate analyses in the experimental study of Huang et al. [6]. The expressions and constants for the reaction rates of char gasification, WGS reaction and metal oxide reduction are basically provided in [8]. Partial oxidation of hydrocarbons by Fe₂O₃ is incorporated into the chemical reaction equation according to our previous study [7].

3. RESULTS AND DISCUSSION

3.1 Model validation

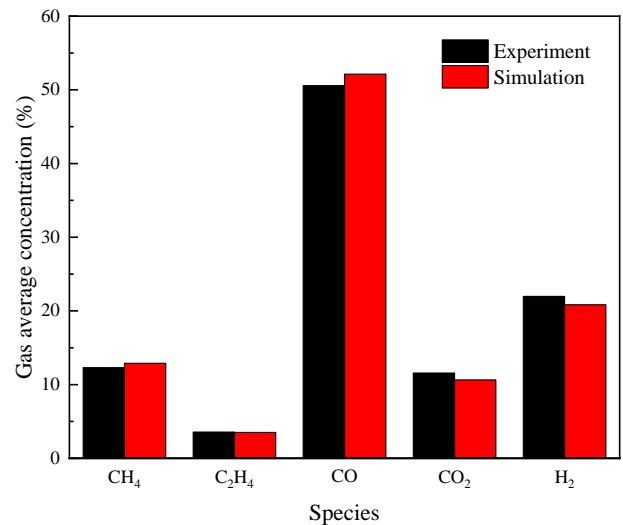


Fig. 1. Comparisons of gas average concentration between simulated results and experimental data.

In order to verify the numerical model, a comparison of the calculated concentration of five gas components and the experimental data is conducted [6], as shown in Fig. 1. It can be seen that a good agreement has been

reached, although the CO concentration is slightly overestimated by 1.6% due to a relatively higher reaction rate assumed for the Boudouard reaction R3, resulting in more CO₂ being converted to CO. Nonetheless, the discrepancy between simulated results and measured values is quite satisfactory, indicating that this model is capable of simulating the biomass CLG fuel reactor with the atmosphere of CO₂, H₂O and their mixture.

Fig. 2 shows the instantaneous contours of volume fractions and velocity vectors for both oxygen carriers and biomass phases at approximately 10 min. It is observed that the biomass is mainly floating near the drop tube inlet due to its low density and the relatively high velocity of the rising gas stream, making this region the primary contact area between volatile gases and metal oxides.

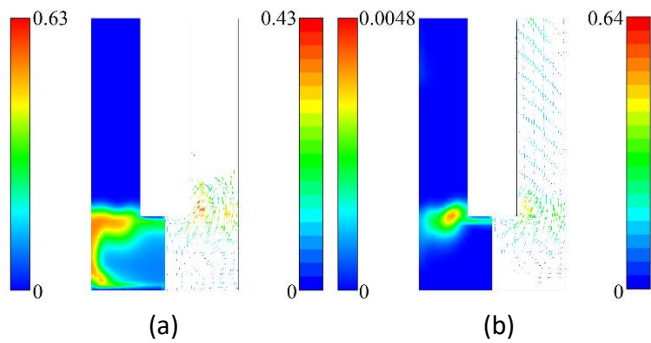


Fig. 2. Contours of volume fractions and velocity vectors (m/s) of oxygen carriers and biomass at $t = 10$ min. (a) Oxygen carriers and (b) Biomass.

3.2 Effects of gasifying agents

The biomass particles experience the thermal degradation once they enter the reactor, releasing the volatiles and producing char and tar. Simultaneously, char is gasified by CO₂ and H₂O via two main gasification reactions R3 and R4. During the simulation with various gasification atmosphere, the feeding rate of biomass and volume flow rate of fluidizing gas were kept constant. The time variation of total amount of char mass within the reactor for different cases (Fig. 3) demonstrates that the char mass of base case is around 3 times that of case 2 and 3, which proves that the addition of H₂O and CO₂ significantly promote the conversion of char into H₂ and CO. Moreover, case 4 displays the fastest consumption rate of char, suggesting the synergistic effect of CO₂/H₂O mixture in the gasification process. Similar results have been presented in literature [3,10]. In addition, char mass displays an increasing trend in all cases. This is because the mass fraction of Fe₂O₃ is descending,

resulting in the decrease of the generation of gasifying agents from the metal oxide reduction reactions.

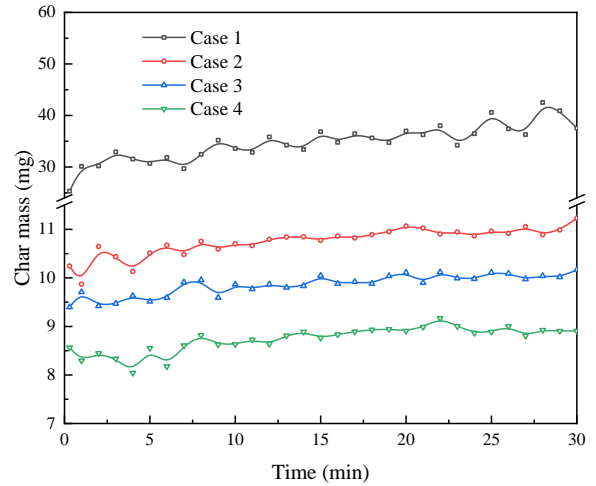


Fig. 3. Total amount of char mass within the reactor versus time for different cases.

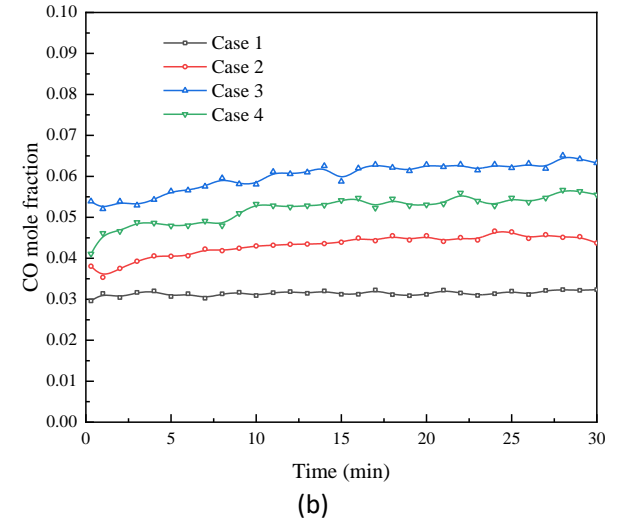
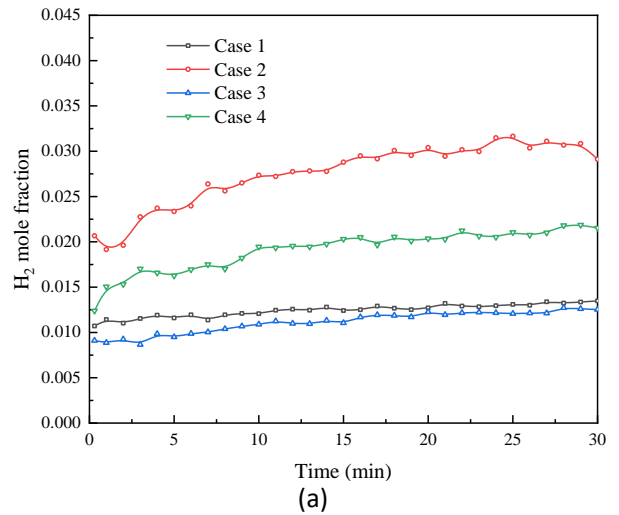


Fig. 4. Product gas mole fractions at the outlet of the reactor versus time for different cases. (a) H₂ and (b) CO.

CO and H₂ are two primary product gases in the gasification system. Fig. 4 shows the mole fractions of these two compositions at the outlet of the reactor as a function of time for different cases. The generation of both CO and H₂ are increased with the atmosphere containing H₂O (50% in case 2 and 25% in case 4), owing to the steam gasification reaction R4. However, the outlet mole fraction of H₂ is a bit lower in case 3 with the atmosphere of 50% CO₂ and 50% Ar than that in the base case with 100% Ar. This is attributed to the excessive CO₂ which is more conducive to the reverse reaction of R5, hence more H₂ is converted into H₂O in case 3. However, the total gas yield of CO and H₂ of case 2-4 are still significantly higher than that of the base case, as shown in Fig. 5. Both H₂ and CO production are elevated in the presence of steam while the CO₂ as the gasifying agent only enhances the conversion of char into CO but leads to a slight decrease of H₂ due to the reverse WGS reaction.

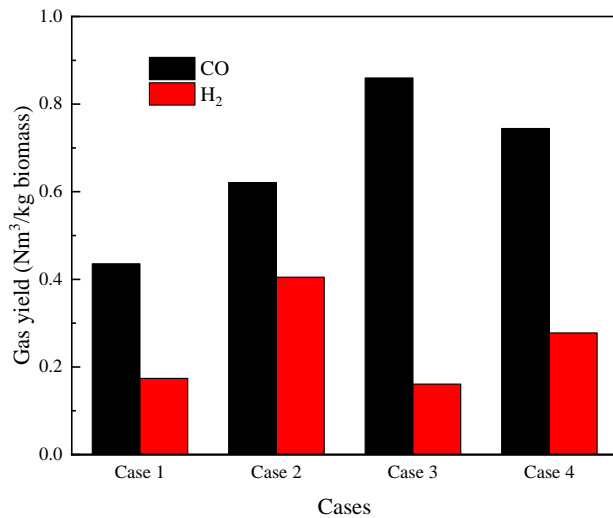


Fig. 5. Calculated gas yield generated from unit mass of biomass for different cases.

4. CONCLUSIONS

Several CFD simulations have been carried out to investigate the effects of various gasification atmosphere on the performance of a biomass CLG reactor based on the experimental study conducted by Huang et al. [6]. The developed model is able to accurately predict the gas concentration for the base case compared to the experimental values and clearly demonstrate the influences of H₂O/CO₂ and their mixture as gasifying agents in the other cases. The results show that the addition of H₂O/CO₂ has a remarkable enhancement on char gasification and indicate that their mixture has synergistic effects in the whole carbon conversion range. According to the outlet mole fractions and gas yields of

the product gases, excess CO₂ has a negative effect on the H₂ production as the reverse WGS reaction is more favorable in such atmosphere.

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