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Research on the Application of Cooling Modules with Inorganic Phase Change Materials in the Thermal Management of Lithium-ion Batteries

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ABSTRACT

Lithium-ion batteries generate a lot of heat during discharge, which can cause the risk of excessive temperature and accelerate the capacity fading rate. Cooling the battery through the latent heat storage of hydrated salt is a good choice. In this study, hydrated salts mixed with sodium acetate trihydrate and disodium hydrogen phosphate dodecahydrate were modified to change the phase change temperature and enthalpy, and then the battery cooling modules were prepared by using modified composite phase change material as a filler and copper foam as a support matrix. The thermal performance of the modified composite phase change material was tested and analyzed by differential scanning calorimetry (DSC) test. The DSC analysis showed that the composite phase change material with 5wt% sodium acetate trihydrate had the best performance, the enthalpy was 278.9 kJ/kg and its phase change temperature was 46.9 °C. The results of the surface temperature measurement experiments of the cooling module on the battery showed that the cooling module can effectively reduce the temperature in the discharge process and the maximum temperature reduction can be up to 9 °C. The lowest temperature was 55 °C with the battery cooling module on the discharge at 1.5C.

Keywords: hydrated salts, phase change material, battery cooling modules, Lithium-ion battery

1. INTRODUCTION

Nearly 30% of global greenhouse gas emissions come from conventionally-fueled road transport and

contribute to air quality and environmental problems worldwide [1]. The focus of research has therefore turned to clean energy vehicles, which operate without harmful substances being released directly into the environment. The energy storage in electric vehicles is electrochemical batteries, with lithium-ion batteries being the most used today. Lithium-ion batteries are promising candidates for their high energy density, low self-discharge rate, long cycle life and high discharge voltage [2-4]. During vehicle use, the battery discharges and generates considerable heat due to the electrochemical reactions in the battery. Therefore, the heat generated by the battery needs to be discharged to maintain the safe operating temperature allowed for the battery [5, 6]. Early studies have shown that if the temperature of a Li-ion battery exceeds 50 °C, the life cycle and rechargeability of the battery is significantly reduced [7]. Safe operating temperatures are typically reported to be within the range of 20-40 °C [8]. Higher temperatures in a battery can reduce its cycling performance and lead to thermal runaway and eventually battery explosion. The maximum temperature difference range should be limited to 5 °C when the battery is in operation [9]. The battery pack may face several problems, such as overcharging, over discharging or short-circuiting due to uneven charging or discharging of the battery. In addition, temperature inhomogeneity increases with increasing discharge rate [10].

The thermal problems associated with safe battery operating conditions described above have been addressed by the use of a Battery Thermal Management System (BTMS). In most cases, the design of the BTMS varies depending on the workpiece used to dissipate the heat from the battery. Many studies have reported on

battery cooling with air and liquid as the cooling media [11-13]. Some of the issues associated with air/liquid cooled BTMS are the need for air/liquid distribution systems, pumping accessories and power consumption [14]. The application of phase change materials in BTMS reduces the complexity of the system components. Al-Hallaj and Selman [15] first introduced the concept of phase change regulation in cell cooling and showed a reduction in cell temperature and a better uniformity of temperature in the cell. They also studied cylindrical cells analytically and estimated the reduction in cell temperature in the cooling system employed by PCM. Analysis of the ageing behavior of PCM-cooled prismatic cells has been reported by Rao et al. [16]. khateeb et al. [17] presented simulation results for a Li-ion battery module operating at a higher ambient temperature of 40°C. At an initial temperature of about 25°C, the temperature rise was up to 40°C, similar to the wide range of ambient temperatures from 20°C to 55°C proposed by Fathabadi [18], where a comparison of combined PCM cooling in free convection and forced convection modes shows that such a system can limit the temperature to below 60°C.

Some researchers have also used multiple layers of phase change materials to cool the batteries [19, 20]. Although it has been effective in cooling down the batteries, it is mainly organic phase change materials that are used. Organic phase change materials also suffer from leakage problems and most applications require additional wrapping material on the outside, thus drastically reducing the thermal conductivity. Organic phase change materials have the disadvantage of being flammable and can easily cause fires when thermal runaway occurs in the battery. The use of inorganic phase change materials has therefore become a new research direction [21, 22]. The main inorganic phase change materials are hydrated salts, whose heat of phase change depends on the strength of bonding between separated water molecules [23]. The phase change temperature of hydrated salts can range from a few degrees Celsius to over 100 °C. The main hydrated salt phase change materials include magnesium chloride hexahydrate [24], sodium sulphate decahydrate [25, 26], sodium carbonate heptahydrate [27] and sodium acetate trihydrate [28]. However, most phase change materials inevitably suffer from phase changes, supercooling and lower thermal conductivity during phase change. Different additives and controlled mass fractions are added to improve the properties [29].

Sodium acetate trihydrate (SAT) has received increasing attention among phase change energy storage

materials [30-32] due to its suitable phase change temperature (58.4°C) and high latent heat of phase change (264 kJ/kg). It is also characterized by a low coefficient of phase change expansion, good chemical stability, non-toxicity and low cost. Not surprisingly, as a hydrated salt phase change material, SAT suffers from high subcooling, phase delamination, low thermal conductivity (0.4~0.7W/(m·K)) [33-35] and corrosion with commonly used metals (copper, aluminium, stainless steel) [36]. A great deal of work has been done in the preparation of composite phase change materials. Different nucleating agents, thickeners and phase change thermoregulators have been experimentally selected for application to SAT matrices to overcome these problems to some extent [37-39].

Based on this research background, this paper attempts to prepare composite phase change materials (CPCM). The thermal properties of the new composites were investigated by experimentally applying disodium hydrogen phosphate dodecahydrate (DHPD) to the SAT combines. The composite phase change materials were added to copper foam and the whole was used as a battery cooling module (BCM) in temperature control experiments for battery discharge in order to determine their applicability in BTMS. The present study provides practical guidance for the design and optimization of thermal management structure for Lithium-ion batteries.

2. EXPERIMENTAL

2.1 Materials

In the experiments, SAT, DHPD, aluminum oxide nanoparticles and carboxymethyl cellulose (CMC) supplied by Shanghai Maclean Company were selected for blending. The copper foam used in this experiment was supplied by Suzhou Jiaside Metal Foam Co. We chose a copper foam with a porosity of 85% and a pore density of 50 ppi. The square battery used in this experiment was purchased from Tianjin Shenli Co., the exact dimensions of which are indicated in Fig. 2. The batteries are rated at 4.4V and have a total capacity of 4590mAh.

2.2 Preparation method

All substances were accurately weighed and mixed. For experimental accuracy, the mass of each sample was set at 20 g. The proportions of the components in the samples are shown in Table 1 and the required mass of each substance was weighed on an electronic balance. SAT was first added and stirred and heated for 10 minutes, then DHPD was added, mixed and heated again

for 10 minutes and finally alumina nanoparticles and CMC were added, each sample was heated uniformly in an oil bath maintained at 110 $\,^{\circ}$ C. The stirrer was kept in the flask at 1100 r/min to ensure the samples were well mixed and the beaker was sealed during this process. Finally, the samples were cooled and solidified at room temperature.

In order to cool down the battery, the copper foam is cut into squares of 25 mm on each side and the thickness of the copper foam is uniformly 5 mm. The melt impregnation method was used to prepare a battery cooling module (BCM) containing a composite phase change material. The preparation process is illustrated in Fig. 1.

Table 1 Components of composite phase change materials

Component	SAT	DHPD	CMC	Nano Al ₂ O ₃
Sample	(w%)	(w%)	(w%)	(w%)
S1	0.00	91.50	3.50	5.00
S2	5.00	86.50	3.50	5.00
S3	45.75	45.75	3.50	5.00
S4	51.50	40.00	3.50	5.00
S 5	71.50	20.00	3.50	5.00
\$6	81.50	10.00	3.50	5.00
S7	84.00	7.50	3.50	5.00
\$8	86.50	5.00	3.50	5.00
S9	91.50	0.00	3.50	5.00

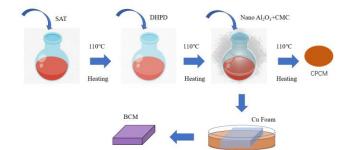


Fig. 1. Process for the preparation of CPCMs and BCMs

2.3 Characterizations

The phase change behavior of the worthy composite phase change material was characterized using a differential scanning calorimeter (Netzsch DSC-200PCPhox, Germany) at a heating level of 2 °C/min. All tests are carried out at room temperature and in a nitrogen-protected environment.

The temperature of the surface of the cell was measured by means of a T-type thermocouple, as shown

in Fig. 2. Five measurement points (a, b, c, d, e) were set up on the cell, at the two pole lugs and at each quarter of the cell. The temperature of the discharged surface of the cell at different multiplier conditions was measured both before and after the placement of the phase change cooling module. The entire experiment was carried out at an ambient temperature of 25 $\,^{\circ}$ C.

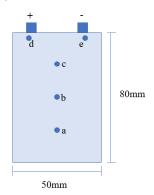


Fig. 2. Battery parameters and thermocouple position

3. RESULTS AND DISCUSSION

3.1 Thermal properties

Nine sets of samples from S1 to S9 were obtained by adjusting the ratio of SAT and DHPD components in the composite phase change material. The enthalpies of these nine samples were examined and the phase change parameters obtained are listed in Table 2. The measured DSC results are shown in Fig. 3.

It is clear from Fig. 3 that there are two distinct peaks at low levels of SAT, indicating that two substances are present separately and that there are substances undergoing phase change processes at different temperatures. When the mass fraction of SAT reaches 71.5%, there is only one melting peak left on the curve, which can prove that the phase change behavior of SAT has completely influenced the change process of DHPD.

Of the nine samples, S1 and S9 did not have the largest enthalpies, but S2 had the largest enthalpy of 278.9 kJ/kg and the phase change onset temperature of the S2 sample was 46.9 °C. After S2, the enthalpy of the composite phase change materials generally tended to increase, but S7 showed a sudden drop, indicating that although the effect of DHPD on the melting peak was negligible at this point, the enthalpy of the composite phase change materials was not as high as the enthalpy of S2. The effect on the enthalpy is much greater.

As the phase change temperature point of sample S2 is near the battery alert temperature of 45 $\,^{\circ}$ C and the enthalpy of the composite phase change material is also

at its maximum at this time, the composite phase change material required for the copper foam based BCM was chosen to be prepared in the proportions corresponding to S2.

Table 2 Phase change parameters of CPCM

	Onset	End	Phase
Come ml -		-	change
Sample	temperature	•	enthalpy
	T _{mo} (℃)	$T_{me}(^{\circ}C)$	(kJ/kg)
S1	50.3	57.3	159.6
S2	46.9	52.5	278.9
S3	46.5	54.6	164.9
S4	44.4	52.3	179.1
S 5	57.4	65.1	212.1
S6	55.8	70.5	219.0
S7	59.3	67.1	192.5
S8	57.6	67.3	230.2
S9	56.0	68.8	235.4

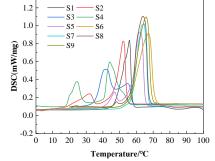


Fig. 3. Enthalpy result curves for samples S1 to S9.

3.2 Battery thermal management behaviors

Due to the need for stable battery operation, there is a risk that the battery will stop working and explode if the temperature exceeds 45 $^{\circ}\mathrm{C}$ during battery discharge. As shown in Fig. 4, the surface temperature variation of a battery discharged at different multipliers without the addition of the BCM is shown. It can be seen that as the magnification increases, the surface temperature of the battery also increases.

As can be seen in Fig. 4(a), the maximum temperature on the surface of the battery already reaches 45 $^{\circ}\mathrm{C}$ at 0.7 C. In picture b, where the battery is discharged at 1.0 C magnification, the surface temperature of the battery rises to 57 $^{\circ}\mathrm{C}$ and exceeds 45 $^{\circ}\mathrm{C}$ before the battery has been discharged for more than the usual length of time. In figure c, at the end of the discharge process, the battery temperature reaches

65 $^{\circ}$ C and in figure d, the maximum temperature reaches 70 $^{\circ}$ C.

A comparison of the four Fig. 4(a) to (d) graphs shows that the difference in temperature between the battery surfaces is not large, with a maximum temperature difference of 4 $\,^{\circ}\mathrm{C}$, and that the temperature difference gradually increases as the discharge multiplier increases. What can be noticed is that the greatest increase in battery surface temperature is seen from 0.7 C to 1.0 C, with the cell surface temperature increasing from 45 $\,^{\circ}\mathrm{C}$ to 57 $\,^{\circ}\mathrm{C}$, an increase of 12 $\,^{\circ}\mathrm{C}$, while from 1.0 C to 1.3 C the temperature increases by 8 $\,^{\circ}\mathrm{C}$ and from 1.3 C to 1.5 C the temperature increases by just 5 $\,^{\circ}\mathrm{C}$.

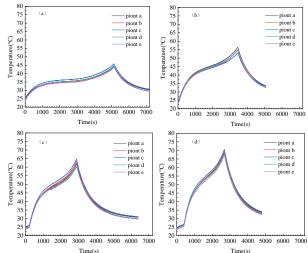


Fig. 4. Surface temperature curves of the battery without BCM at 0.7C (a), 1.0C (b), 1.3C (c) and 1.5C (d).

During the discharge of the battery a huge amount of heat is generated, causing the surface temperature of the battery to rise rapidly in a short period of time [40]. A cooling module is therefore placed on the surface of the battery in the hope that it will help to alleviate the rapidly rising surface temperature.

The maximum surface temperature of the battery at the end of the discharge in Fig. 5(a) did not exceed 45 $^{\circ}$ C, and the maximum temperature in Fig. 5(b) is 48 $^{\circ}$ C, the battery is basically discharged within the safe temperature. The maximum surface temperature of the battery is reduced by 9 $^{\circ}$ C. The maximum temperature at the end of discharge in Fig. 5(c) is 58 $^{\circ}$ C, which is a reduction of 7 $^{\circ}$ C compared to the case without the cooling module. Fig. 5(d) shows that the maximum temperature was 65 $^{\circ}$ C and the temperature was reduced by 5 $^{\circ}$ C compared to the case without the presence of the BCM.

As can be seen from figure a, the BCM is not effective in cooling the highest temperature point of the battery at 0.7 C, but the temperature in all other shops is

reduced to around 35 $^{\circ}$ C, keeping the battery at an optimum temperature of 35 $^{\circ}$ C throughout the discharge process [41]. The minimum temperature on the surface of the battery at the end of discharge in Fig. 4(b) is 40 $^{\circ}$ C, the minimum temperature on the surface at the end of discharge in Fig. 4(c) is 50 $^{\circ}$ C and the minimum temperature on the surface at the end of the discharge process in Fig. 4(d) is 55 $^{\circ}$ C.

By comparing the minimum temperature at the surface of the battery with and without the BCM, it can be seen that the BCM reduces the surface temperature of the battery to a large extent at each discharge multiplier, quickly absorbing the heat generated during the discharge of the battery. With the BCM survived, the battery is able to operate safely at discharge multipliers less than 1.0 C, and at multipliers greater than 1.0 C it can significantly reduce the surface temperature of the battery.

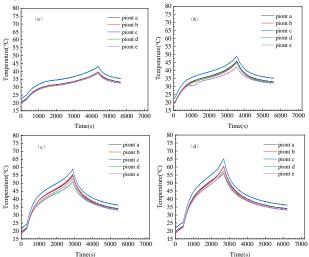


Fig. 5. Surface temperature curves of the battery with BCM at 0.7C (a), 1.0C (b), 1.3C (c) and 1.5C (d).

4. CONCLUSION

In this paper, a variety of inorganic phase change material composites with copper foam as the substrate, were used to investigate the cooling of the battery cooling. The main conclusions are summarized below.

- (1) At a SAT mass fraction of 5%, the CPCM can achieve a maximum phase change enthalpy of 278.9 kJ/kg and a phase change temperature of 46.9 $\,^\circ\mathrm{C}$.
- (2) Without the presence of the BCM, the maximum temperature of the battery discharged at 1.0 C is 57 $\,^{\circ}$ C, which is above the warning temperature, and the maximum surface temperature of the discharged at 1.5 C can reach 70 $\,^{\circ}$ C.
- (3) With the addition of the BCM, the surface temperature of the battery at the end of discharge is

significantly reduced. The maximum surface temperature is reduced by up to 9 $^{\circ}$ C with a maximum temperature of 65 $^{\circ}$ C.

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