

Investigation of a Novel Net-Zero Polygeneration System for Power, Hydrogen and Ammonia Production

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ABSTRACT

This study investigates a novel net-zero polygeneration system for the production of power, hydrogen, and ammonia. The integration of oxy-combustion, an alkaline electrolyzer, and ammonia synthesis via the Haber-Bosch process significantly enhances the efficiency of individual components and the overall system showcasing its potential for developing more sustainable and efficient energy solutions.

Keywords: polygeneration system, power production, hydrogen, ammonia, process simulation

NONMENCLATURE

Abbreviations

ASU	Air Separation Unit
NZC	Net Zero Cycle
ACM	Aspen Custom Modeler
FC	Fractional conversion

Symbols

\dot{m}	Mass flowrate
\dot{W}	Power

1. INTRODUCTION

Anthropogenic CO₂ emissions from the power, hydrogen, and ammonia production industries have significantly contributed to climate change, underscoring the urgent need for sustainable production methods [1, 2]. In power production sector, oxy-combustion utilizes nearly pure oxygen, obtained through an air separation unit (ASU), allowing for easier separation of CO₂ from effluent and achieving net-zero CO₂ emissions [3]. Allam Cycle, also referred as NZC (Net Zero Cycle), shows the highest efficiency of the power production among other methods of the power production [4]. Hydrogen serves

as both an energy carrier and a vital feedstock for various processes, including ammonia production [1]. It is notable for its high energy density and zero-emission potential when produced from renewable resources, making it an essential component of sustainable energy systems [5]. Currently, the majority of hydrogen production is obtained through Steam Methane Reforming (SMR), which generates what is termed "gray hydrogen." This process emits significant amounts of CO₂ into the atmosphere, contributing to environmental damage [6, 7]. As a result, utilizing renewable resources to produce green hydrogen should be considered to reach sustainable hydrogen production. Alkaline electrolyzers utilizing renewable resources are known for their reliable performance, high efficiency, quick dynamic response, and ability to produce green hydrogen with satisfactory purity [8]. In addition, ammonia holds great promise for a low-carbon future, with a volumetric energy density of 12.7 MJ/L—three times higher than compressed hydrogen at 69 MPa and 25°C, and about ten times greater than lithium-based batteries [9]. Ammonia production is essential for the fertilizer industry and is also recognized as an efficient energy carrier and fuel [10]. Polygeneration processes, which produce electricity, heat, and chemicals simultaneously, boost resource efficiency and reduce environmental impact by integrating energy systems, resulting in lower emissions and resource use [11]. This study explores the integration of oxy-combustion, hydrogen, and ammonia production, demonstrating the potential for developing more efficient and sustainable energy systems. Both the individual processes and the overall integrated system are studied.

2. MATERIAL AND METHODS

Fig. 1 illustrates the proposed polygeneration system for producing power, hydrogen, and ammonia. The study utilized the process simulator Aspen Plus V.14, licensed by Aspen Tech. Alkaline electrolyzer was modeled in Aspen Custom Modeler (ACM) according to [12-14] study, and imported to Aspen Plus while other unit operations were simulated with Aspen Plus in-built unit operations. Alkaline electrolyzers are typically operated at temperatures between 70 and 140°C, with pressures ranging from 15 to 30 bar, using an aqueous KOH solution at a concentration of 25-35 wt% [15, 16].

NZC is favored for oxy-combustion power generation, as it is widely regarded as the most efficient method for producing power in such processes [17]. The combustor is modeled using an RGibbs reactor with 3% excess O₂, and the combustion temperature is regulated by the recycling streams. The 15-stage cooled turbine is modeled based on El-Masri's continuous expansion model [4]. The regenerators are modeled as multi-stream heat exchangers, with a minimum temperature difference of 20°C in the "Top regenerator" and 5°C in the "Bottom regenerator". Additionally, temperature crossover is monitored by dividing both regenerators into 50 zones. An air separation unit (ASU), with an energy consumption of 1365 kJ/kg_{O₂} [4], is simulated as a black-box model. It supplies part of the oxygen needed for combustion, nitrogen for the ammonia-synthesis process, and provides excess heat to both regenerators. A carbon sequestration unit is integrated into the process to capture a portion of the generated CO₂, proportional to the fuel's mass flow rate, in order to prevent the direct release of CO₂ into the atmosphere. A portion of the electricity generated in the NZC is used to power all the turbomachinery in the system, while the remaining electricity is considered the net power production.

Ammonia is produced through the Haber-Bosch process, combining hydrogen and nitrogen in a 3:1 ratio [18]. Ammonia synthesis is an exothermic reaction [19], and a three-stage cascade process is being explored to enhance system efficiency through effective heat integration. By utilizing the heat generated in each stage, this approach aims to improve overall energy efficiency and performance in ammonia production. The ammonia reactors are modelled using REquil reactor.

3. THEORY AND CALCULATION

In this study, following assumptions have been made:

1. The system is simulated and analyzed under steady-state conditions.
2. Pressure losses in the system's piping are neglected.
3. The electrolyzer is powered by firm renewable energy sources.
4. The minimum operating temperature of the system is set to 26°C.

Heat integration promotes process efficiency by optimizing energy use [20]. Considering original NZC system layout [21], the top and bottom regenerators are modified to harness excess heat from the ammonia synthesis and electrolyzer outlet streams. This effective heat utilization minimizes the reliance on cooling utilities in the hydrogen and ammonia production subsystems, enhancing overall efficiency. Moreover, the condensed water from the NZC is already deionized, allowing it to be directly used as feedwater for the electrolyzer, thereby removing the need for a desalination unit. In the stand-alone NZC layout, the primary role of ASU is to produce oxygen using air, while nitrogen typically being released into the atmosphere. However, with the current system design and integration, the nitrogen generated by the ASU can be redirected into the ammonia synthesis process. This eliminates the need for a distinct ASU unit for large-scale ammonia production or pressure swing adsorption for medium-scale operations. The sizes of these three systems are determined so that no additional O₂ from the electrolyzer and ASU, nor extra N₂ generated by the ASU, remain. Additionally, the net mole flow rates of ammonia and hydrogen production are balanced.

This study employs the first law of thermodynamics to assess the efficiency of individual processes, such as the NZC, hydrogen production, and ammonia production, as well as the overall system efficiency. The overall efficiency of the polygeneration system is calculated using following equation:

$$\eta_{Polysys} = \frac{(\dot{W}_{gross,turb.} - \dot{W}_{comp.}) + \dot{m}_{H_2,net} \cdot LHV_{H_2} + \dot{m}_{NH_3} \cdot LHV_{NH_3}}{\dot{m}_{fuel} LHV + \dot{W}_{elec.}} \quad (1)$$

In this context, $\dot{W}_{gross,turb.}$ indicates the gross power output produced by the turbine, whereas $\dot{W}_{comp.}$

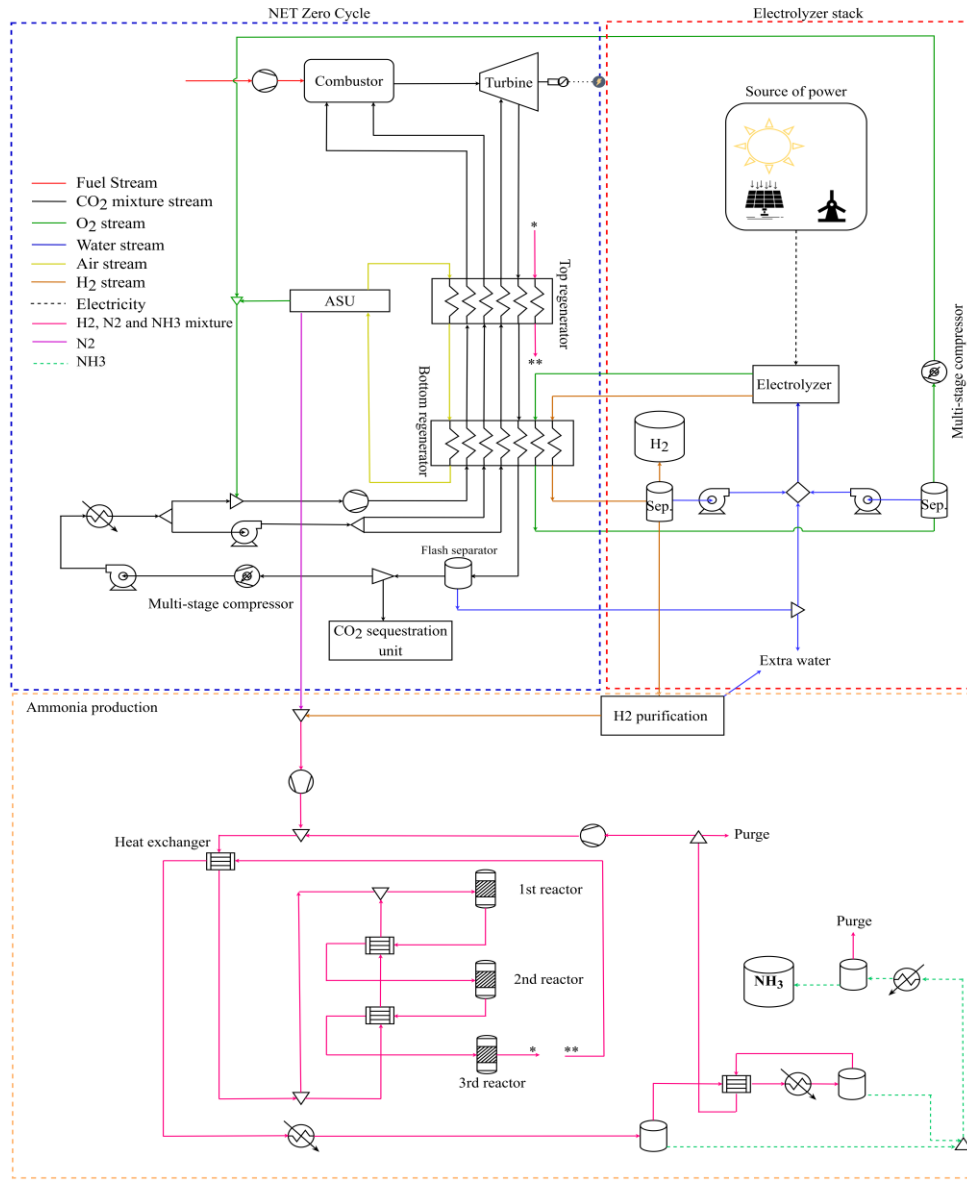


Fig. 1 Layout of the proposed polygeneration system for power, hydrogen, and ammonia production

signifies the total energy consumption of the turbomachinery within the system. The term \dot{m} represents mass flow, LHV stands for the lower heating value, and $\dot{W}_{elec.}$ refers to the renewable energy input used to operate the electrolyzer.

4. RESULTS AND DISCUSSION

Table 1 presents the outcomes of the polygeneration system. As shown, the NZC achieves an efficiency of 66.1%, which is considerably higher than the 54% efficiency of the standalone NZC under the same operating conditions, as reported in [4] study. The

environmental benefit of this improved efficiency means that more electricity is generated without increasing CO₂ emissions, as CO₂ capture remains constant. The condensed water from the NZC subsystem exceeds the amount needed to fully meet the deionized water requirements of the electrolyzer. The ammonia production efficiency is 77.2%, with a purity of 99.9%. During the ammonia synthesis process, the single-pass fractional conversion of hydrogen in the 1st, 2nd, and 3rd reactors is 20.2%, 15.9%, and 12.7%, respectively. However, by recycling the unreacted components and employing effective heat integration, the ammonia yield

increases to 96.2%. This yield surpasses the 94.2% yield reported by [10] study for ammonia production in the polygeneration system. Additionally, the high purity of hydrogen and nitrogen fed into the ammonia process contributes to this elevated yield. Finally, the overall system demonstrates an efficiency of 62.2%. This efficiency should be compared with other polygeneration systems that produce ammonia.

Table 1 Polygeneration system results

Properties	Unit	Polygeneration system
Thermal energy of fuel (LHV)	MW _{th}	768.3
Renewable energy input	MW _e	1186.1
Combustor temperature	°C	1100
Combustor pressure	bar	300
Turbine outlet pressure	bar	34
Turbine power output	MW _e	650.9
Recycle flow energy consumption	MW _e	178.91
NG compressor	MW _e	4.3
Air separation unit	MW _e	8.7
NZC net electric power output	MW _e	507.9
Overall system net power output	MW _e	463.3
Gross hydrogen production rate	kmol/s	3.44
Net hydrogen production rate	kmol/s	1.34
Ammonia production rate	kmol/s	1.34
Hydrogen FC in 1 st reactor	%	20.2
Hydrogen FC in 2 nd reactor	%	15.9
Hydrogen FC in 3 rd reactor	%	12.7
Purity of ammonia production	mole%	99.9
Ammonia production yield	%	96.2
Electrolyzer efficiency (LHV)	%	70.2
NZC efficiency (LHV)	%	66.1
Ammonia production efficiency (LHV)	%	77.2
Overall system efficiency (LHV)	%	62.2

5. CONCLUSION

Integrating the NZC, alkaline electrolyzer, and ammonia production via the Haber-Bosch process not only enhances the standalone efficiency of the NZC and boosts ammonia yield but also results in a highly efficient overall system. This integration increases NZC power production efficiency from 54% to 66.1%. Hydrogen and ammonia can be produced with efficiencies of 70.2% and 77.2%, respectively. From an environmental perspective,

this process results in zero direct CO₂ emissions into the atmosphere, and the deionized water produced by the NZC subsystem completely eliminates the need for a desalination unit.

References

- [1] Pawar ND, Heinrichs HU, Winkler C, Heuser P-M, Ryberg SD, Robinius M, et al. Potential of green ammonia production in India. *International Journal of Hydrogen Energy*. 2021;46:27247-67. DOI: <https://doi.org/10.1016/j.ijhydene.2021.05.203>
- [2] Quadrelli R, Peterson S. The energy-climate challenge: Recent trends in CO₂ emissions from fuel combustion. *Energy Policy*. 2007;35:5938-52. DOI: <https://doi.org/10.1016/j.enpol.2007.07.001>
- [3] Climent Barba F, Martínez-Denegri Sánchez G, Soler Seguí B, Gohari Darabkhani H, Anthony EJ. A technical evaluation, performance analysis and risk assessment of multiple novel oxy-turbine power cycles with complete CO₂ capture. *Journal of Cleaner Production*. 2016;133:971-85. DOI: <https://doi.org/10.1016/j.jclepro.2016.05.189>
- [4] Scaccabarozzi R, Gatti M, Martelli E. Thermodynamic analysis and numerical optimization of the NET Power oxy-combustion cycle. *Applied Energy*. 2016;178:505-26. DOI: <https://doi.org/10.1016/j.apenergy.2016.06.060>
- [5] Dincer I, Rosen MA. Sustainability aspects of hydrogen and fuel cell systems. *Energy for Sustainable Development*. 2011;15:137-46. DOI: <https://doi.org/10.1016/j.esd.2011.03.006>
- [6] Soltani R, Rosen MA, Dincer I. Assessment of CO₂ capture options from various points in steam methane reforming for hydrogen production. *International Journal of Hydrogen Energy*. 2014;39:20266-75. DOI: <https://doi.org/10.1016/j.ijhydene.2014.09.161>
- [7] Ali Khan MH, Daiyan R, Neal P, Haque N, MacGill I, Amal R. A framework for assessing economics of blue hydrogen production from steam methane reforming using carbon capture storage & utilisation. *International Journal of Hydrogen Energy*. 2021;46:22685-706. DOI: <https://doi.org/10.1016/j.ijhydene.2021.04.104>
- [8] Nakajima Y, Fujimoto N, Hasegawa S, Usui T. Advanced Alkaline Water Electrolyzer for Renewable Hydrogen Production. *ECS Transactions*. 2017;80:835. DOI: 10.1149/08010.0835ecst
- [9] Arnaiz del Pozo C, Cloete S. Techno-economic assessment of blue and green ammonia as energy carriers in a low-carbon future. *Energy Conversion and Management*. 2022;255:115312. DOI: <https://doi.org/10.1016/j.enconman.2022.115312>
- [10] Xu C, Liu Y, Zhang Q, Xin T, Zhao R, Wang M, et al. Thermodynamic analysis of a novel biomass polygeneration system for ammonia synthesis and power generation using Allam power cycle. *Energy Conversion and Management*. 2021;247:114746. DOI: <https://doi.org/10.1016/j.enconman.2021.114746>

- [11] Serra LM, Lozano M-A, Ramos J, Ensinas AV, Nebra SA. Polygeneration and efficient use of natural resources. *Energy*. 2009;34:575-86. DOI: <https://doi.org/10.1016/j.energy.2008.08.013>
- [12] Sánchez M, Amores E, Abad D, Rodríguez L, Clemente-Jul C. Aspen Plus model of an alkaline electrolysis system for hydrogen production. *International Journal of Hydrogen Energy*. 2020;45:3916-29. DOI: <https://doi.org/10.1016/j.ijhydene.2019.12.027>
- [13] Sánchez M, Amores E, Rodríguez L, Clemente-Jul C. Semi-empirical model and experimental validation for the performance evaluation of a 15 kW alkaline water electrolyzer. *International Journal of Hydrogen Energy*. 2018;43:20332-45. DOI: <https://doi.org/10.1016/j.ijhydene.2018.09.029>
- [14] Jeddizahed J, Webley PA, Hughes TJ. Integrating alkaline electrolysis with oxyfuel combustion for hydrogen and electricity production. *Applied Energy*. 2024;361:122856. DOI: <https://doi.org/10.1016/j.apenergy.2024.122856>
- [15] Murray JN, Yaffe MR. Testing aqueous caustic electrolyzers at high temperatures. *International Journal of Hydrogen Energy*. 1979;4:193-204. DOI: [https://doi.org/10.1016/0360-3199\(79\)90024-7](https://doi.org/10.1016/0360-3199(79)90024-7)
- [16] Schalenbach M, Kasian O, Mayrhofer KJJ. An alkaline water electrolyzer with nickel electrodes enables efficient high current density operation. *International Journal of Hydrogen Energy*. 2018;43:11932-8. DOI: <https://doi.org/10.1016/j.ijhydene.2018.04.219>
- [17] Allam RJ, Fetvedt JE, Forrest BA, Freed DA. The Oxy-Fuel, Supercritical CO₂ Allam Cycle: New Cycle Developments to Produce Even Lower-Cost Electricity From Fossil Fuels Without Atmospheric Emissions. 2014.
- [18] Bicer Y, Dincer I, Zamfirescu C, Vezina G, Raso F. Comparative life cycle assessment of various ammonia production methods. *Journal of Cleaner Production*. 2016;135:1379-95. DOI: <https://doi.org/10.1016/j.jclepro.2016.07.023>
- [19] Kandemir T, Schuster ME, Senyshyn A, Behrens M, Schlögl R. The Haber–Bosch Process Revisited: On the Real Structure and Stability of “Ammonia Iron” under Working Conditions. *Angewandte Chemie International Edition*. 2013;52:12723-6. DOI: <https://doi.org/10.1002/anie.201305812>
- [20] Kralj AK, Glavič P, Krajnc M. Waste heat integration between processes. *Applied Thermal Engineering*. 2002;22:1259-69. DOI: [https://doi.org/10.1016/S1359-4311\(02\)00047-9](https://doi.org/10.1016/S1359-4311(02)00047-9)
- [21] Allam R, Martin S, Forrest B, Fetvedt J, Lu X, Freed D, et al. Demonstration of the Allam Cycle: An Update on the Development Status of a High Efficiency Supercritical Carbon Dioxide Power Process Employing Full Carbon Capture. *Energy Procedia*. 2017;114:5948-66. DOI: <https://doi.org/10.1016/j.egypro.2017.03.1731>